

Coupling of CFD and a Material model for the assessment of incubation time and erosion rate

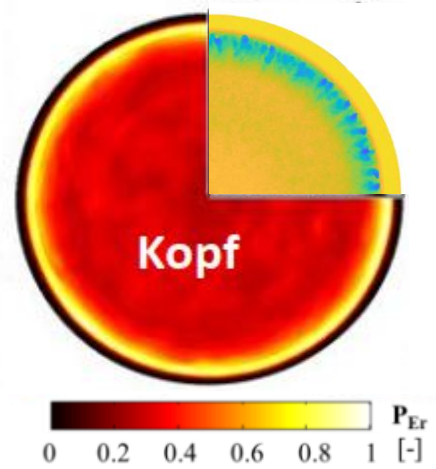
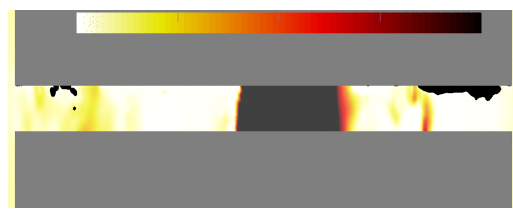
Kavitationsworkshop Drübeck

01.12.2021

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Magnus Haese
Romuald Skoda

- CFD Erosion indicators: Exceeding of **pressure** p and **condensation rate** $\partial\alpha/\partial t$ threshold
- Erosion probability P_{Er} by statistical evaluation
- Assessment of **erosion sensitive wall zones** only, no material information

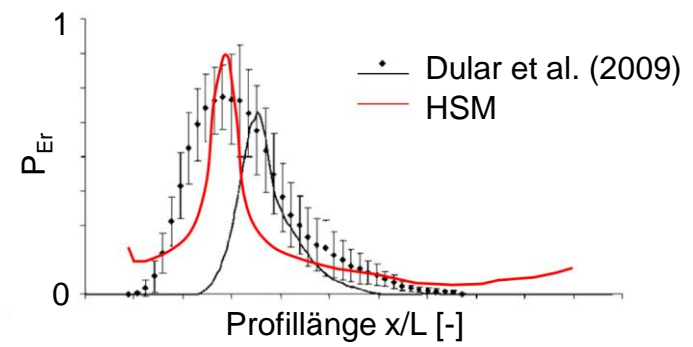
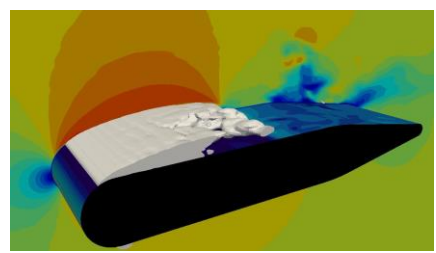
Sonotrode¹⁾



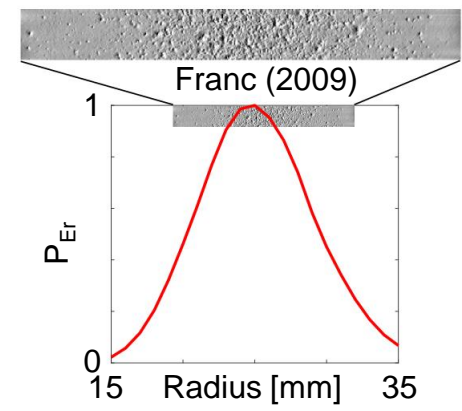
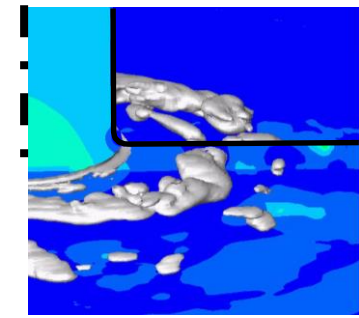
1) Mottyll & Skoda (2016), Ultrasonics Sonochemistry 31, 570–589

3) Mottyll (2018), PhD Thesis

CLE hydrofoil²⁾



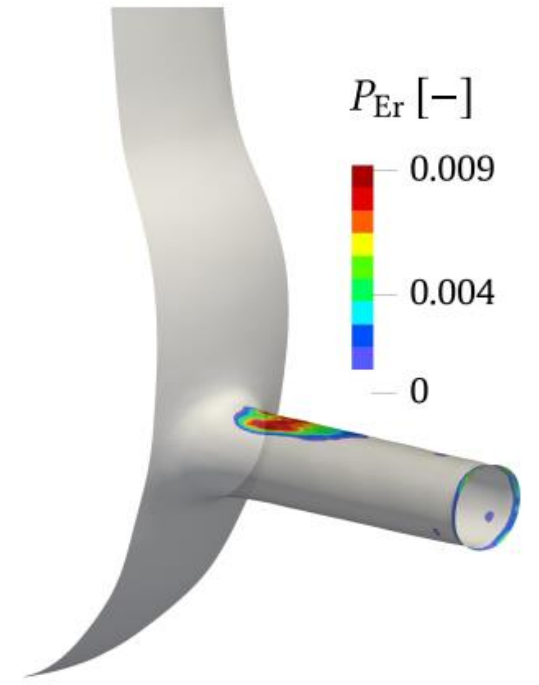
Grenoble case³⁾

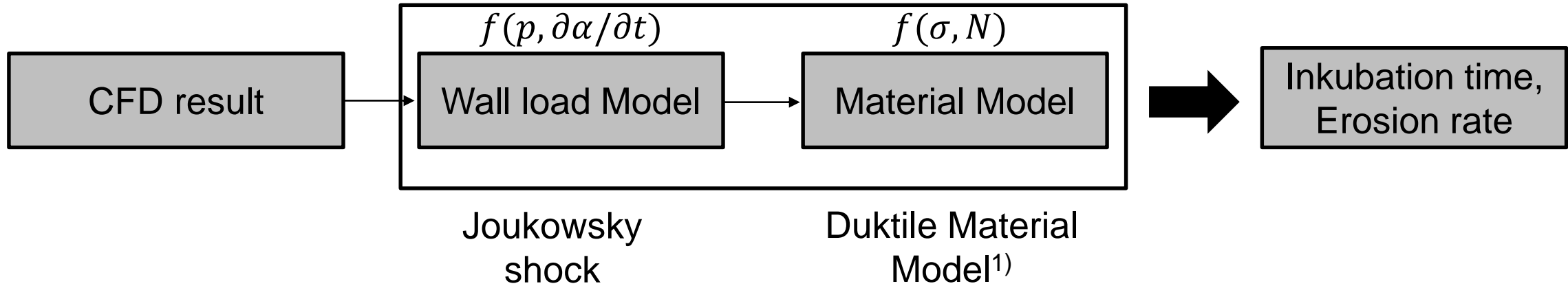


2) Blume & Skoda (2019), Wear 428-429, 457-469

4) Falsafi et al. (2021), Int. J. of Engine Research

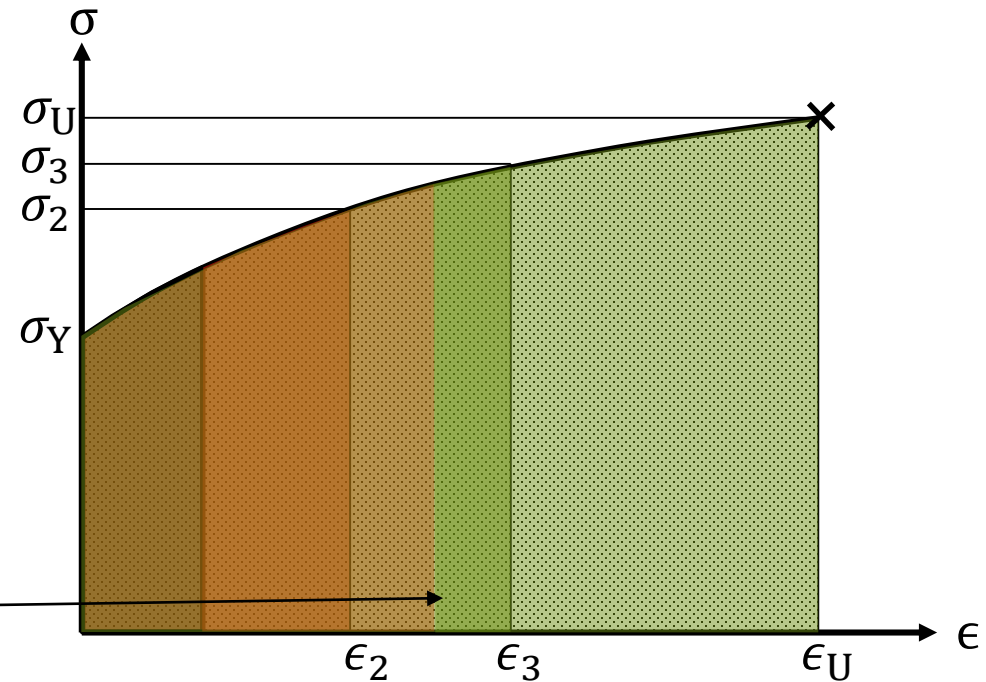
Fuel injector⁴⁾





Material model¹⁾

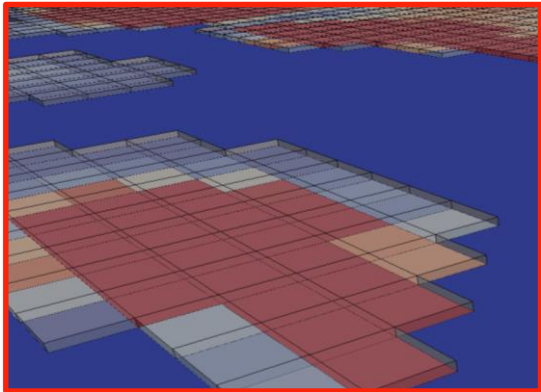
- Accumulation of plastic deformation energy
- Ludwig-type hardening $\sigma(\epsilon) = \sigma_Y + K \epsilon^n$
- Incubation time is reached:



$$W(\sigma_U) \leq \sum W(\sigma_i) = W(\sigma_1) + W(\sigma_2) + W(\sigma_3)$$

Wall load model

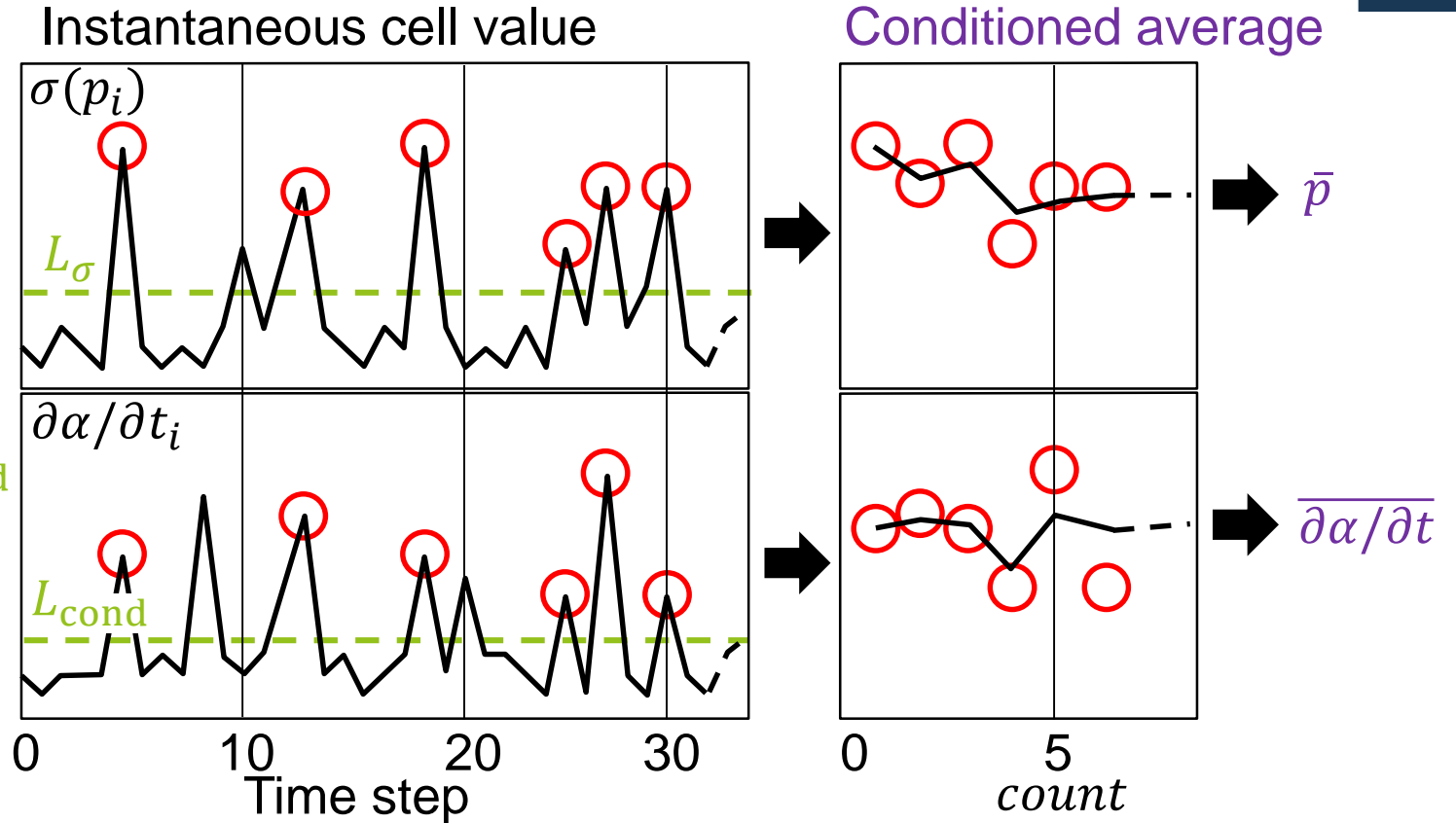
For each wall cell face i



$$\sigma(p_i) > L_\sigma$$

&

$$\frac{\partial \alpha}{\partial t_i} > L_{cond}$$



➤ Wall load

$$c_{jet, Plesset} = 8.97 \cdot \gamma^2 \sqrt{|\bar{p} - p_{sat}| / \rho_l}$$

$$\bar{\sigma} = f(\bar{p}) = \rho_l c_s c_{jet}$$

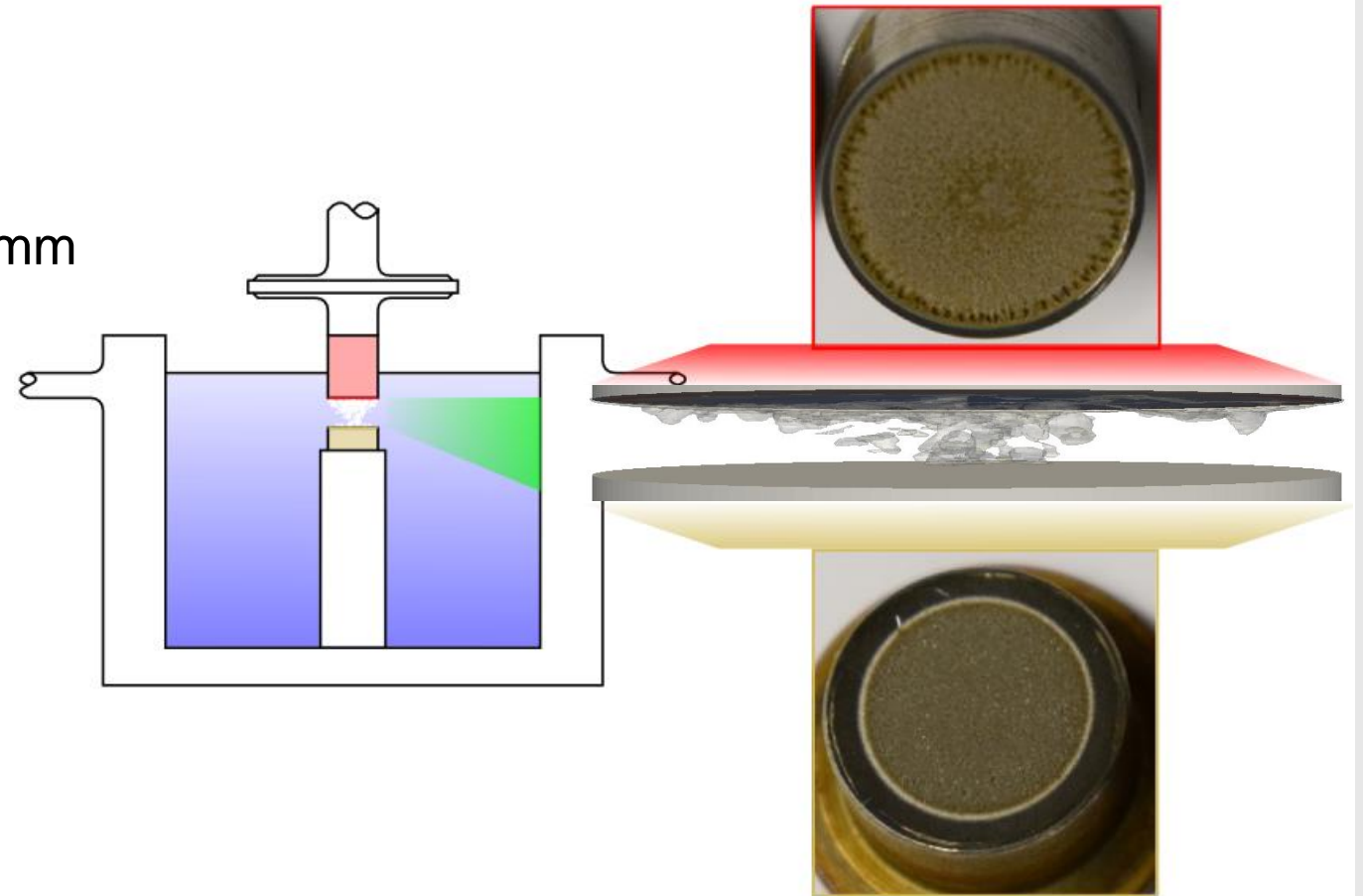
➤ Load rate

$$N = -n_0 \cdot V \cdot \overline{\partial \alpha / \partial t} / A \cdot P_{Er} \cdot F_{cond} \quad P_{Er} = \frac{count \cdot \Delta t}{t_{Sim}}$$

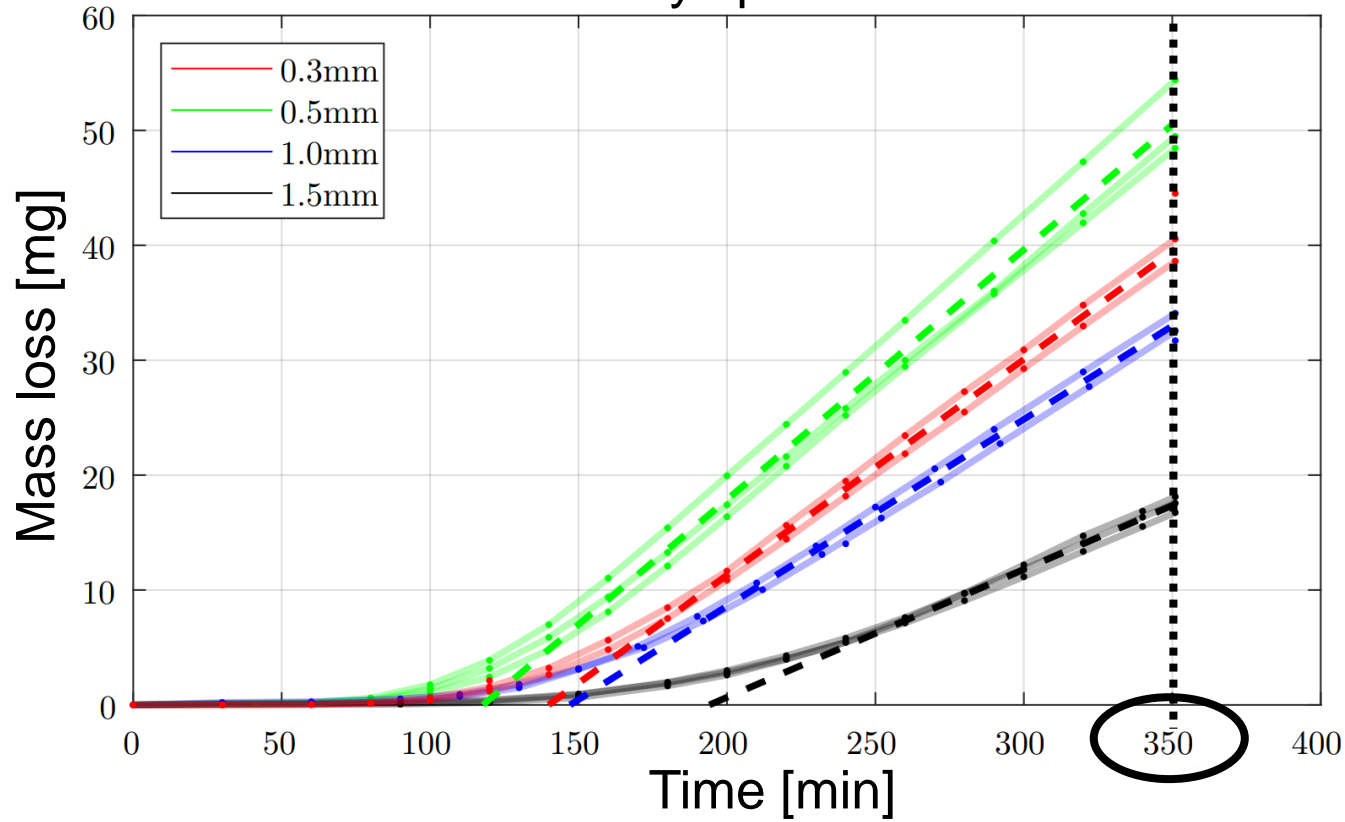
➤ Material model¹⁾: t_{inc} & **MDPR** = $f(\bar{\sigma}, N)$

ASTM G32

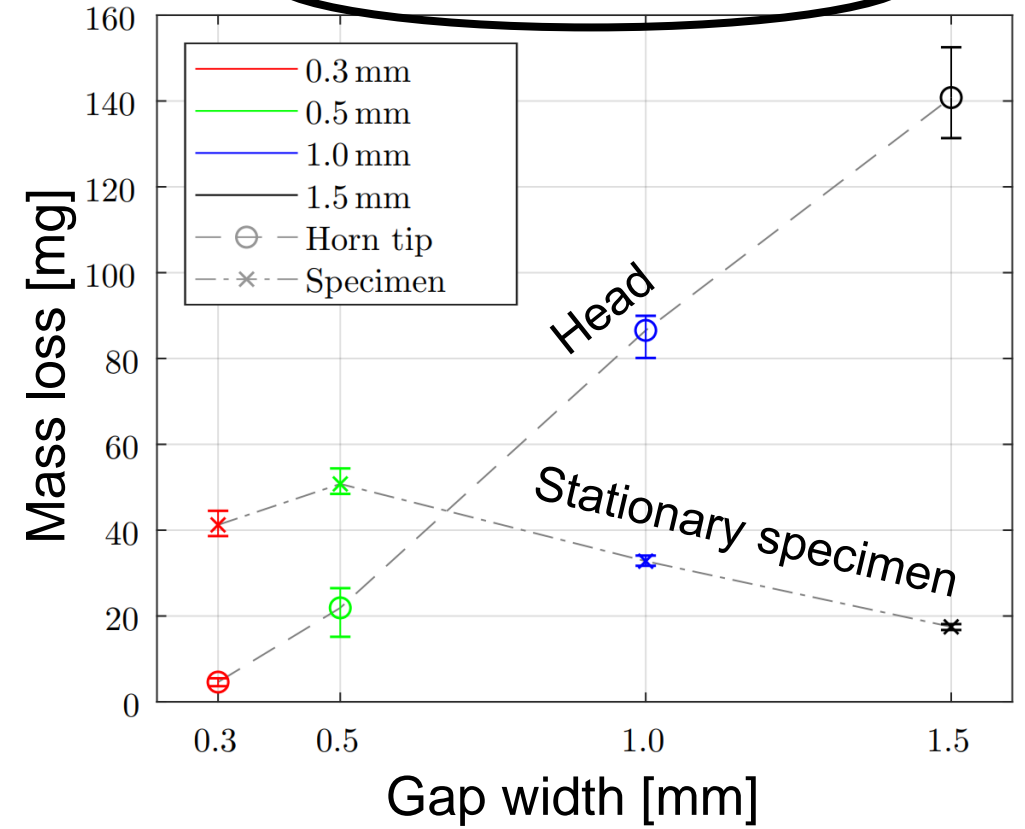
- $f \sim 20\text{kHz}$, $A_{pp} \sim 40\mu\text{m}$
- Gap width variation 0.3; 0.5; 1.0; 1.5mm



Stationary specimen

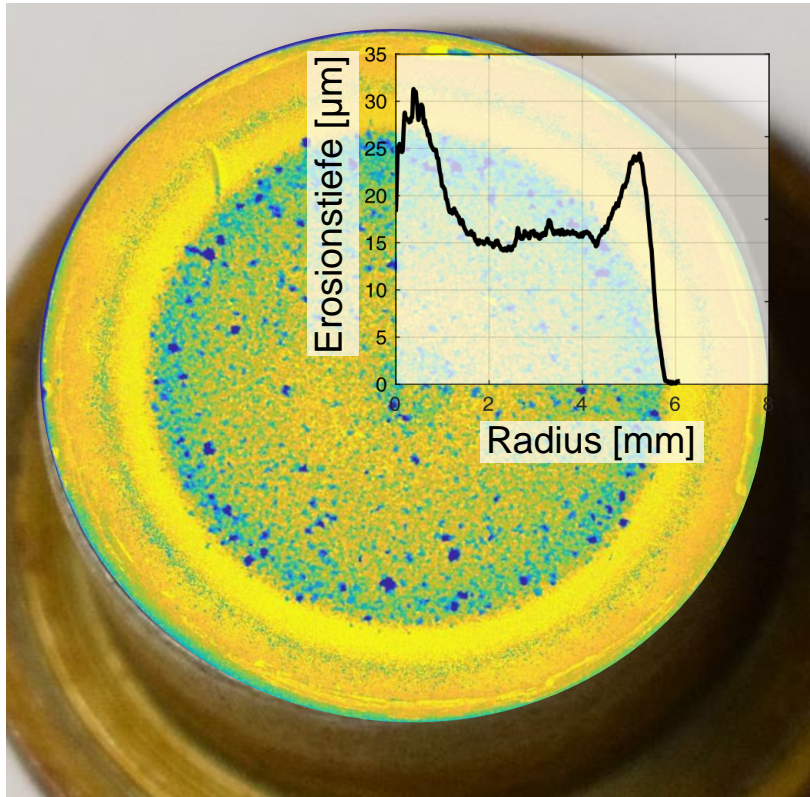


Mass loss after 350min

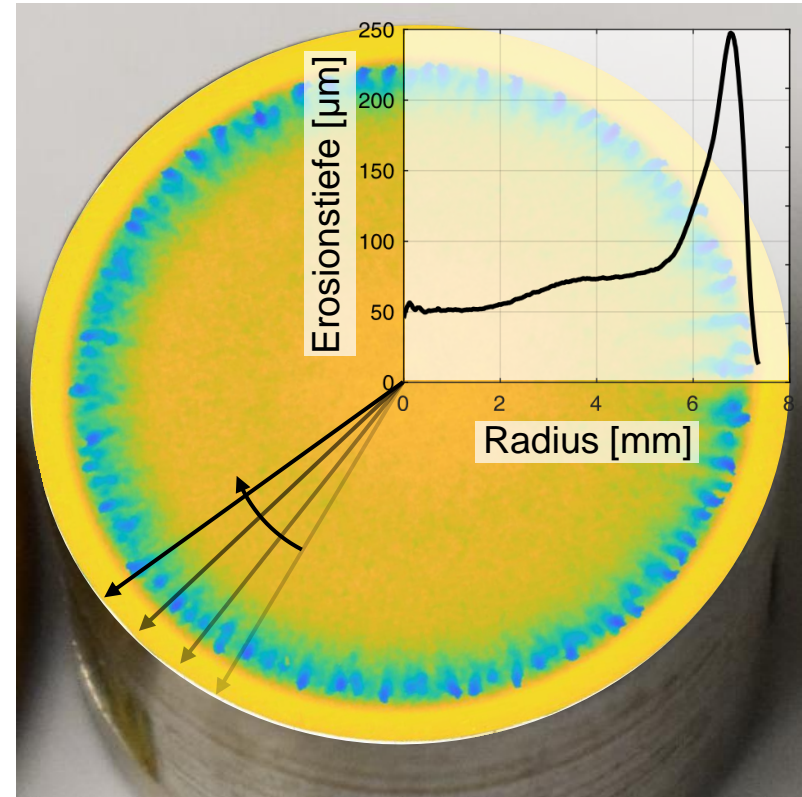


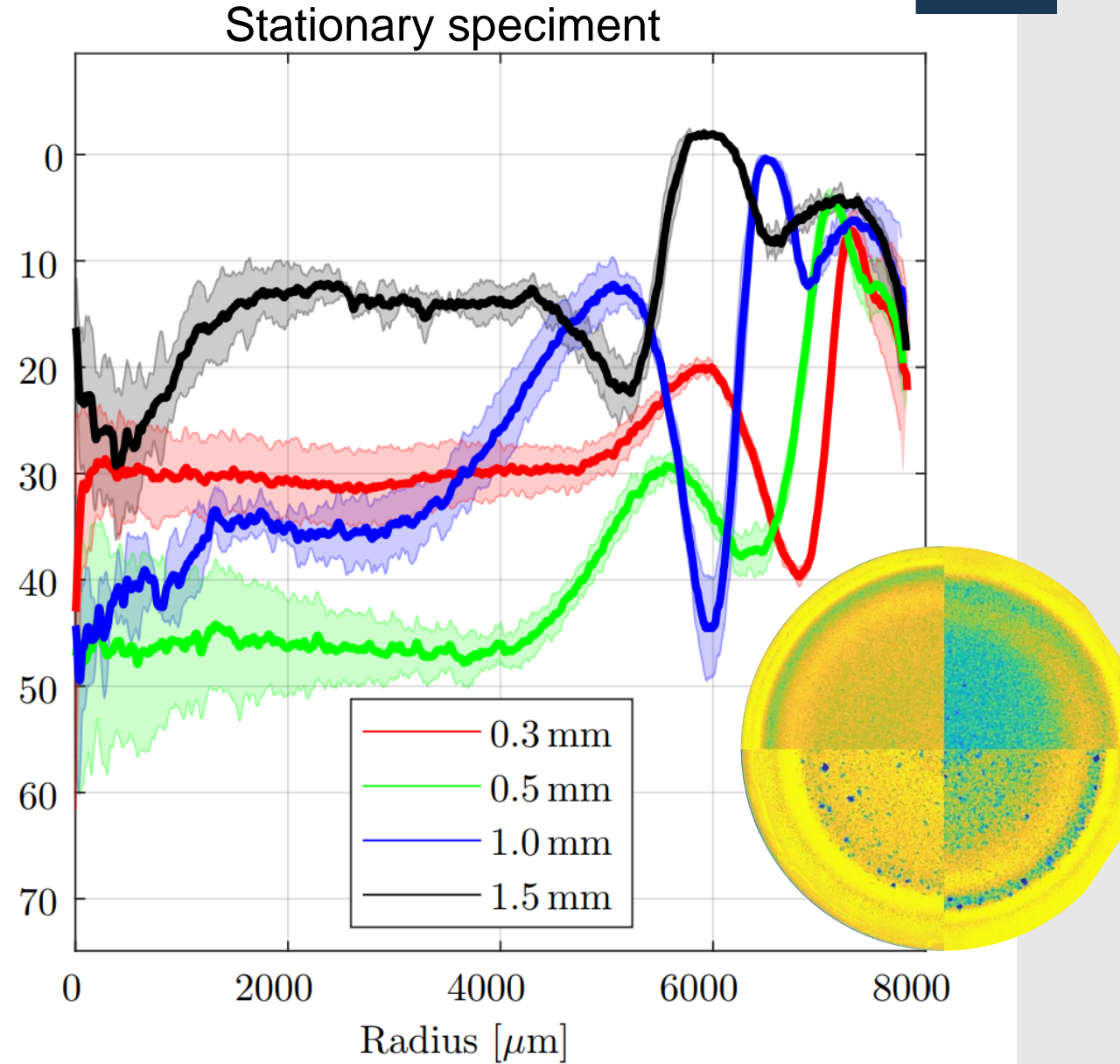
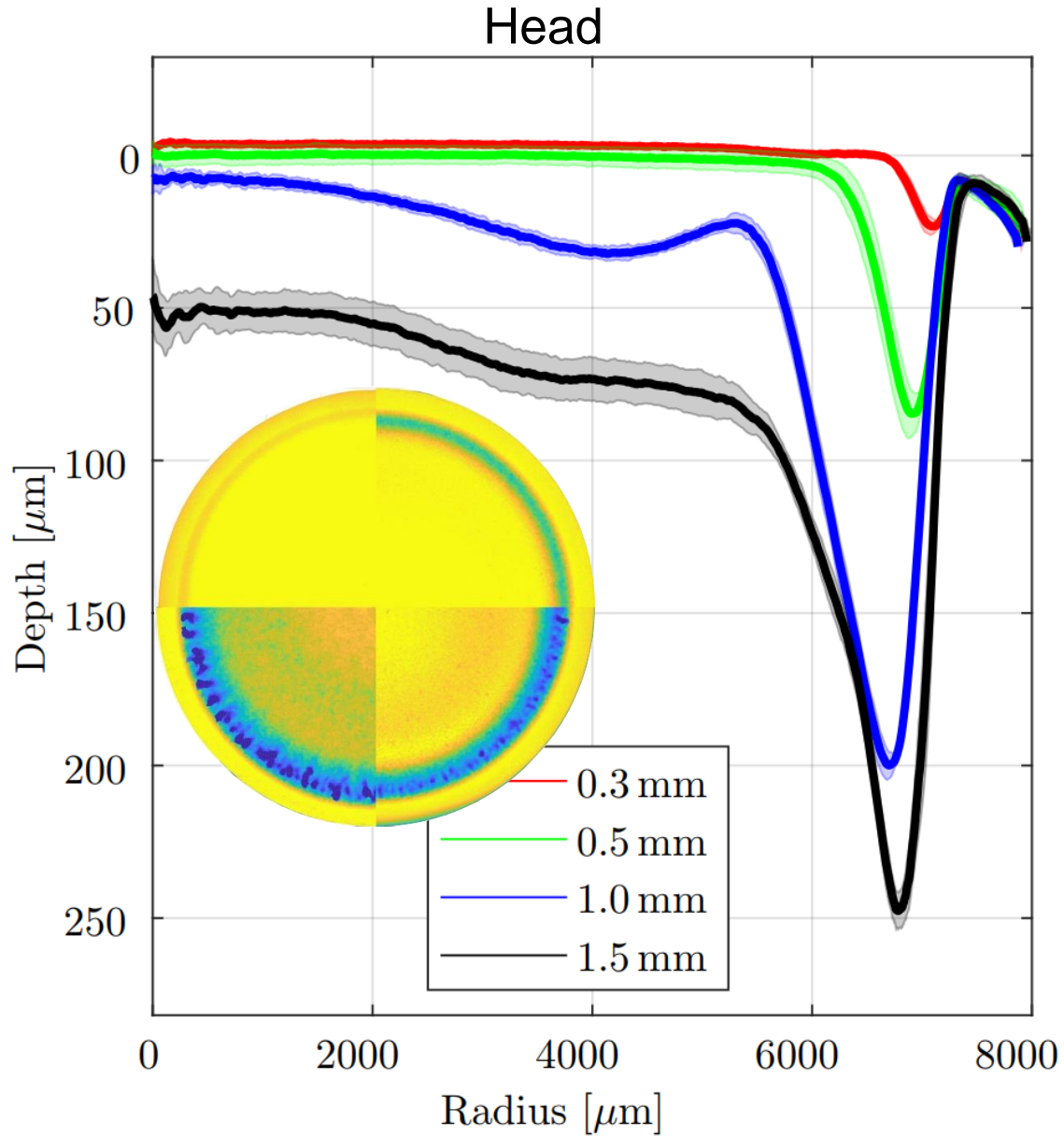
Gap width [mm]	0.3	0.5	1.0	1.5
Incubation time [min]	140	118	147	194
Erosion rate [mg/h]	11.3	13.0	9.8	6.7

Stationary specimen

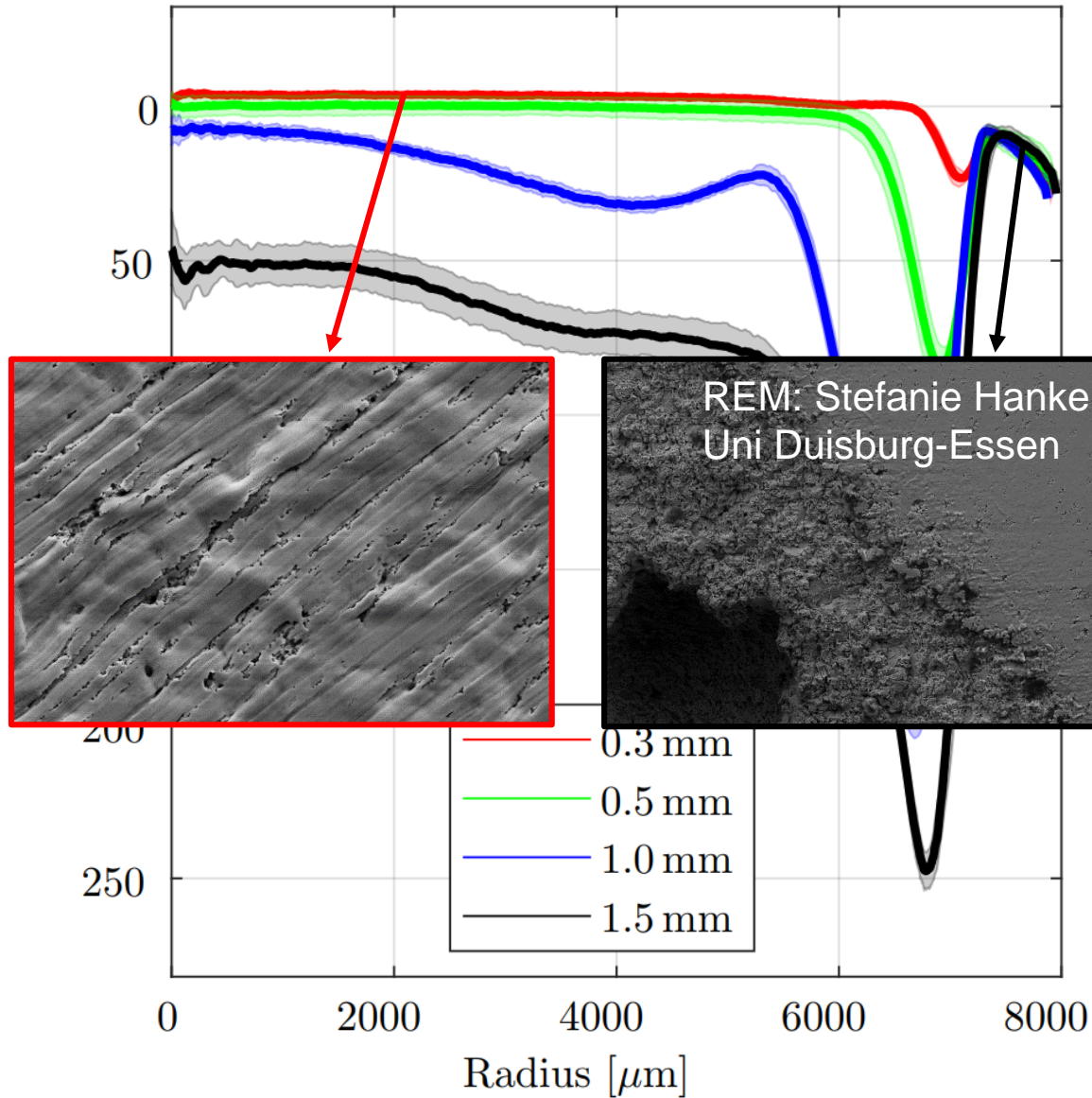


Head

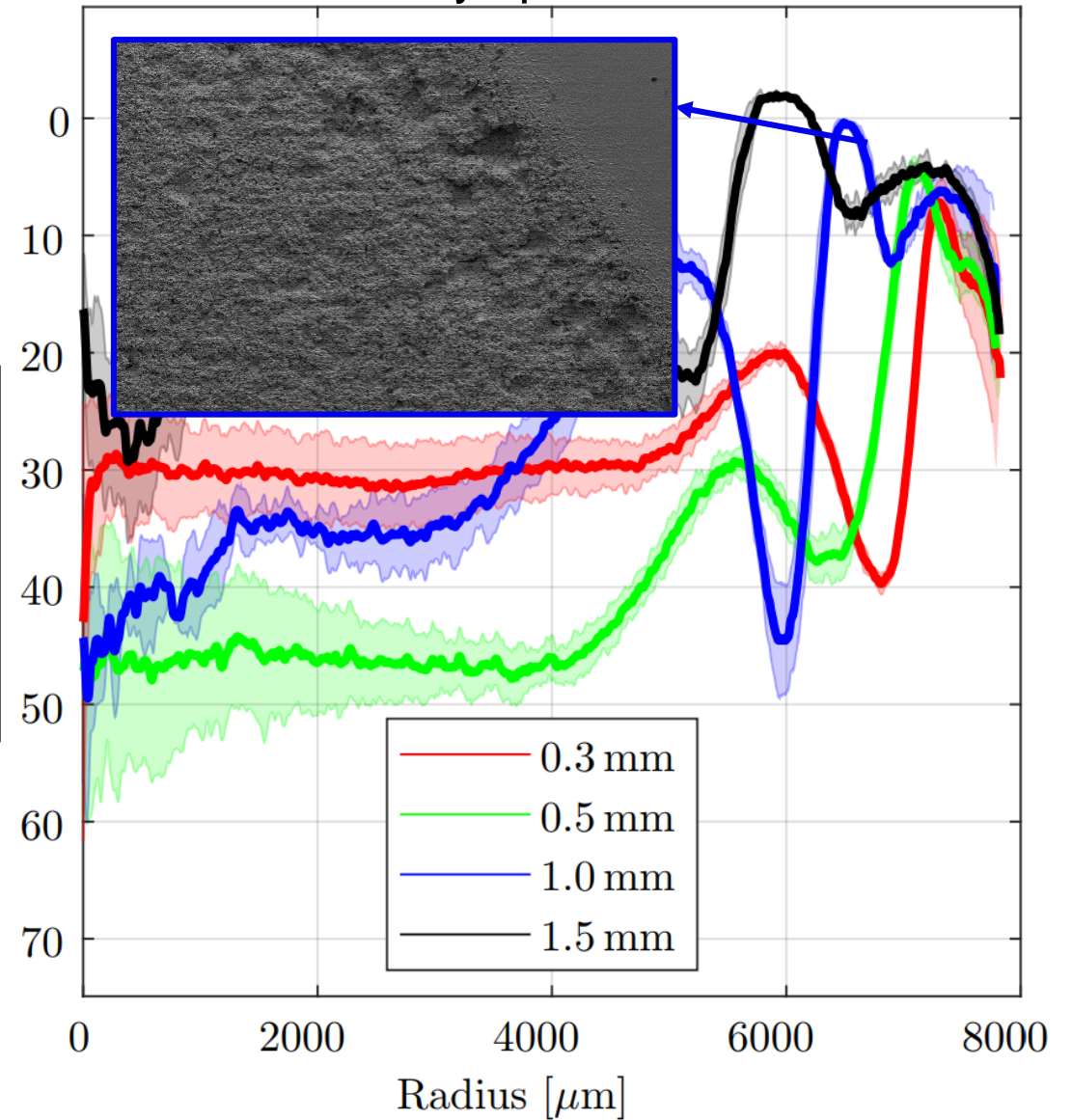




Head

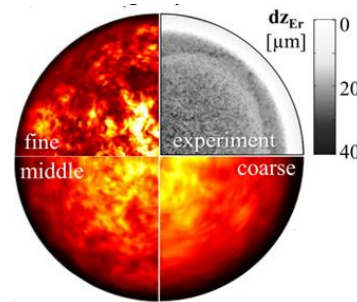


Stationary specimen



hydRUBFoam

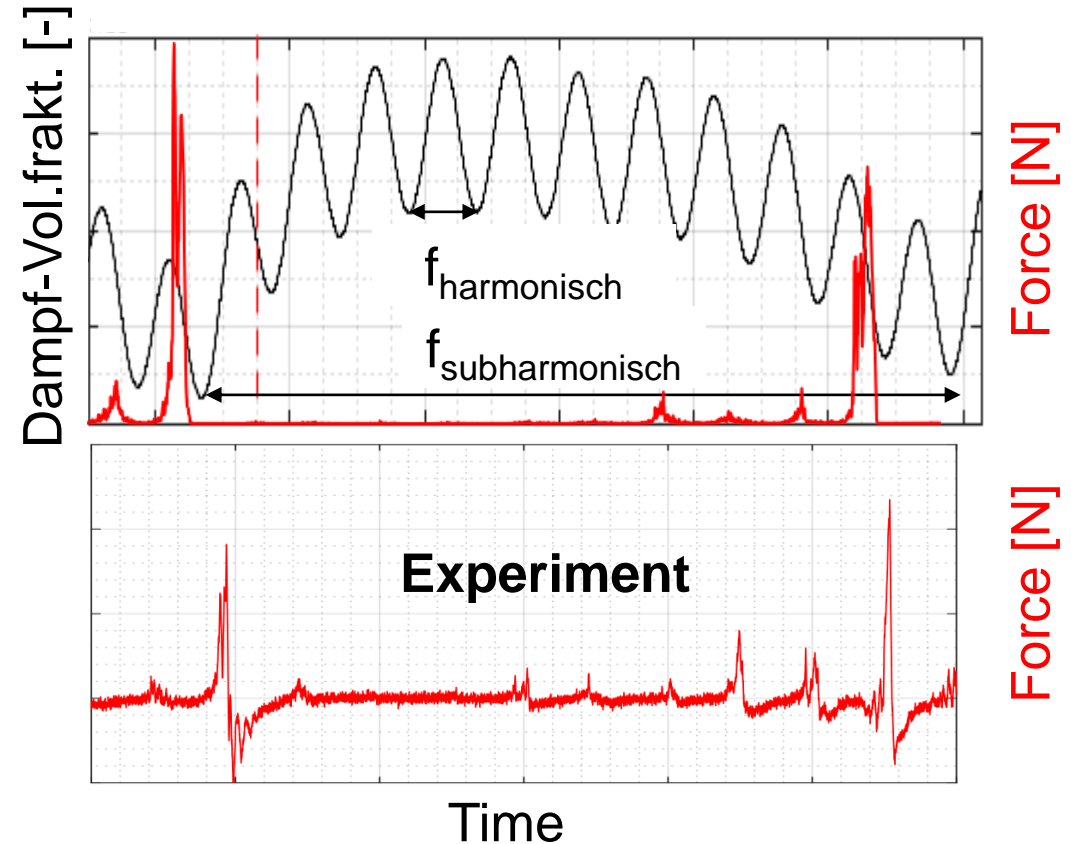
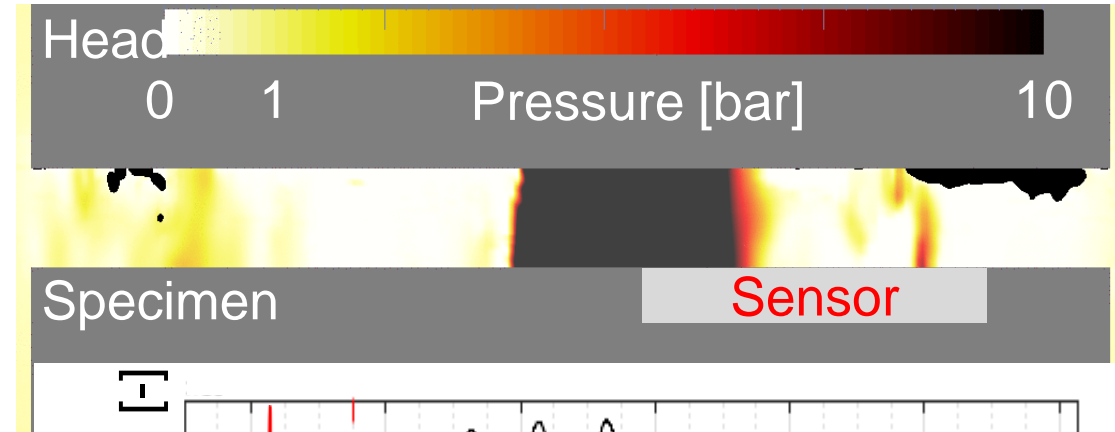
- Compressible, time-explicit density-based non-viscous (Euler) solver
- Shock wave resolution by Riemann solver¹⁾
- Barotropic EOS
- Homogeneous mixture approach
- Harmonic and subharmonic dynamics of Sonotrode are well captured ²⁾ (see rhs)
- Erosion sensitive wall zone capturing ³⁾



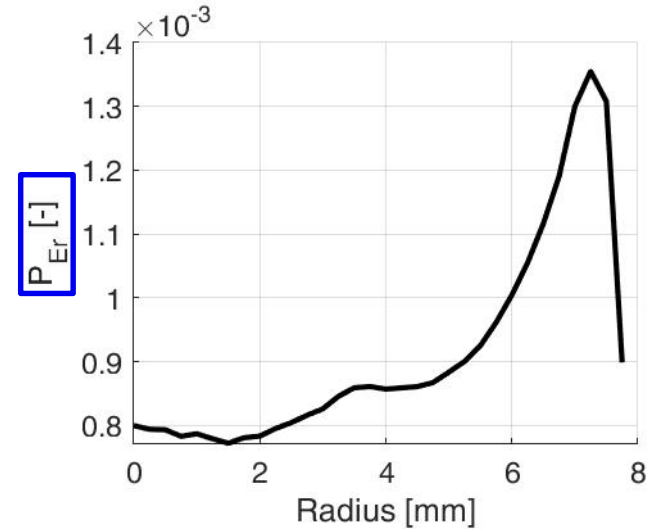
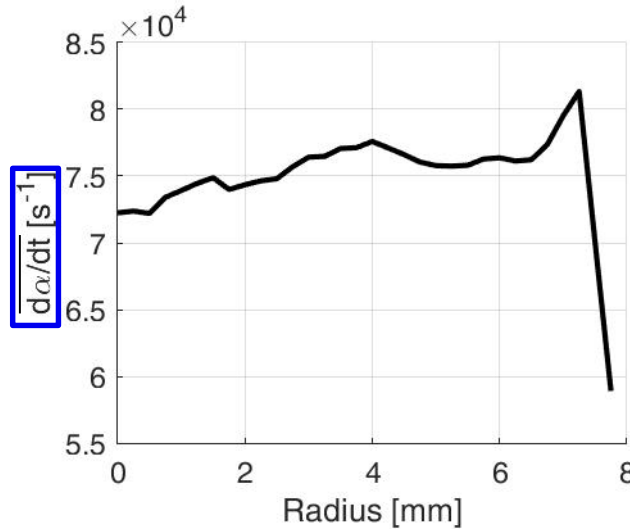
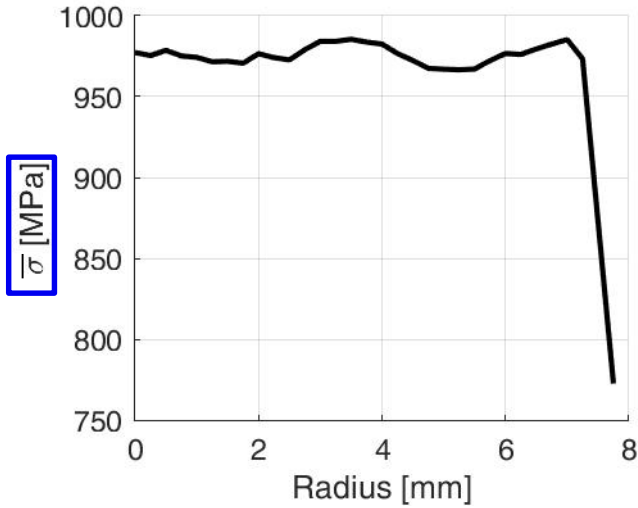
¹⁾ Schmidt et al. (2008), 46th AIAA, paper 2008-1238

²⁾ Schreiner et al. (2019), Ultrasonics Sonochemistry 67, 105091

³⁾ Mottyll & Skoda (2016), Ultrasonics Sonochemistry 31, 570–589



Wall load model



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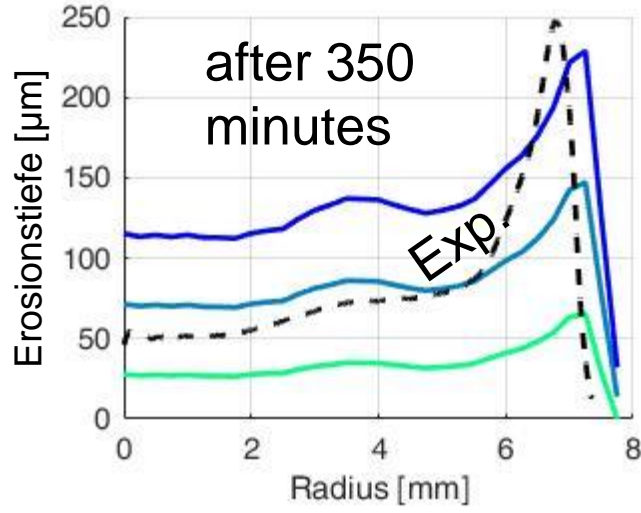
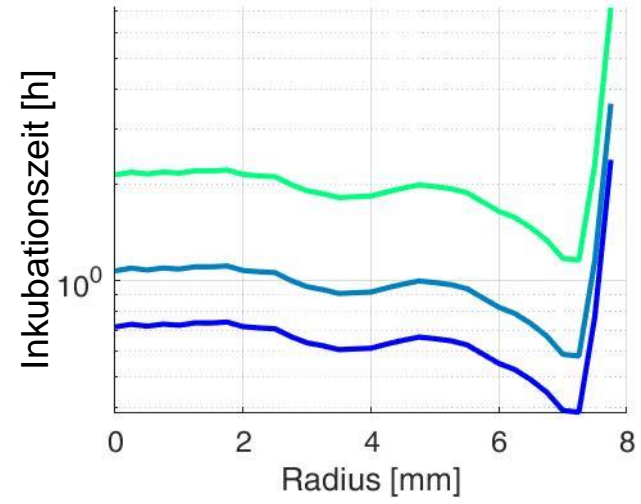
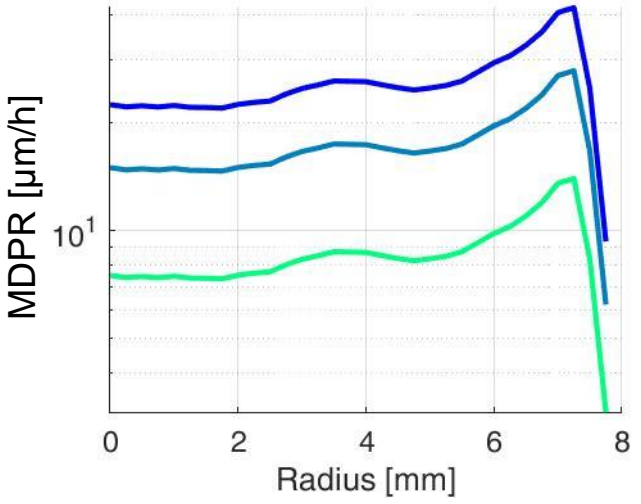
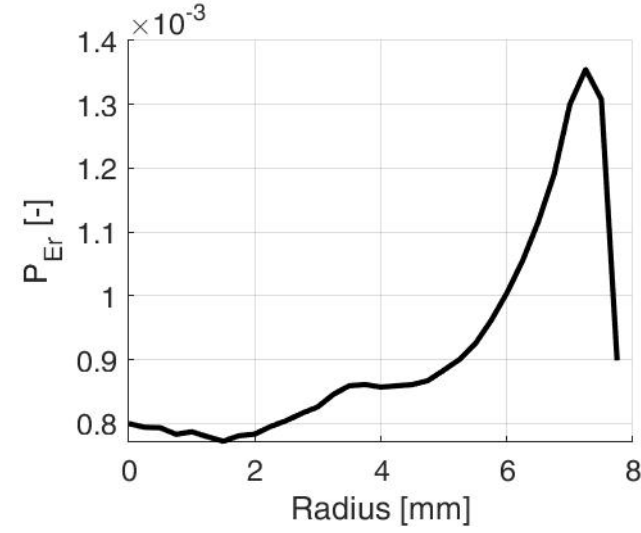
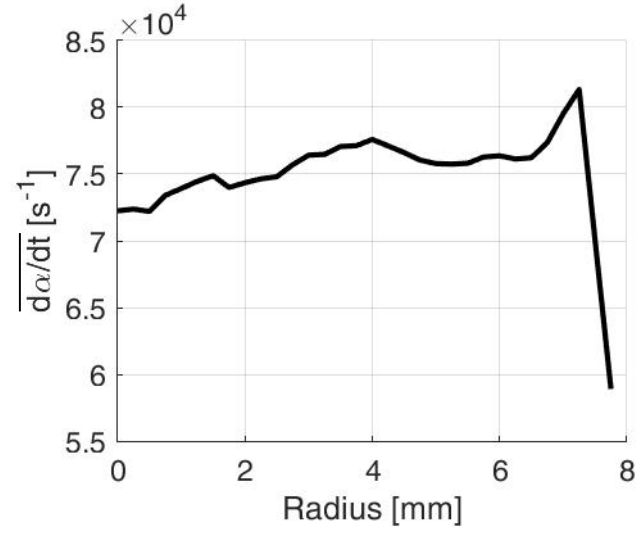
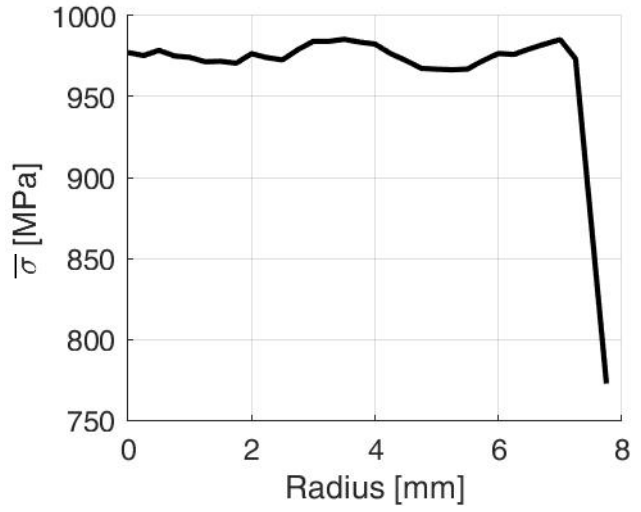
➤ Load rate

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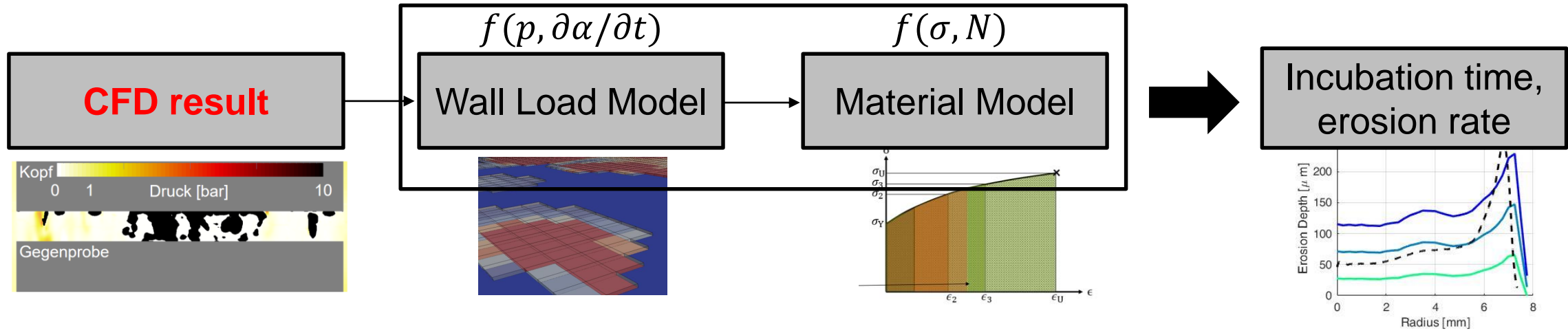
Wall load model



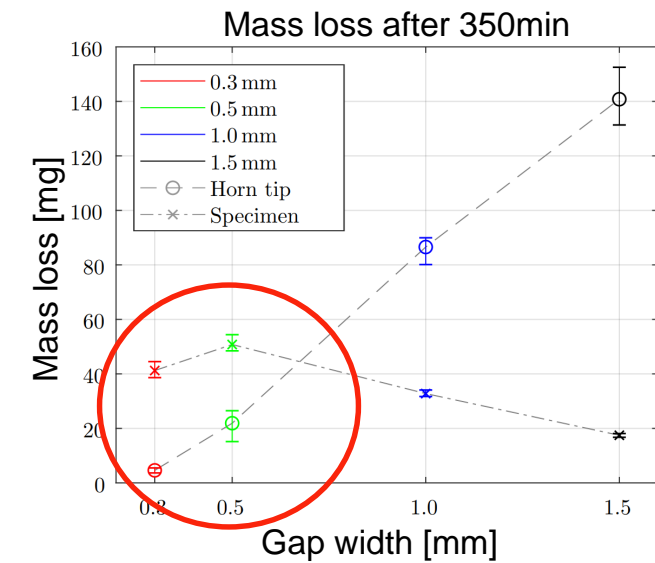
Material model



- $F_{cond} = 1$
- $F_{cond} = 2$
- $F_{cond} = 3$



- Valuable tool in terms of an **extended post-processing**
 - Publication in *Wear* is under preparation
- However: calibration necessary, case dependent
- Sonotrode simulation: **CFD method has still limitations** and is thus restricted to large gap width:
 - Thermal effects
 - Air content



Thank you for your attention!
Thanks to our sponsor for funding.

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